



LightSim : A Leakage Aware Ultrafast Temperature Simulator

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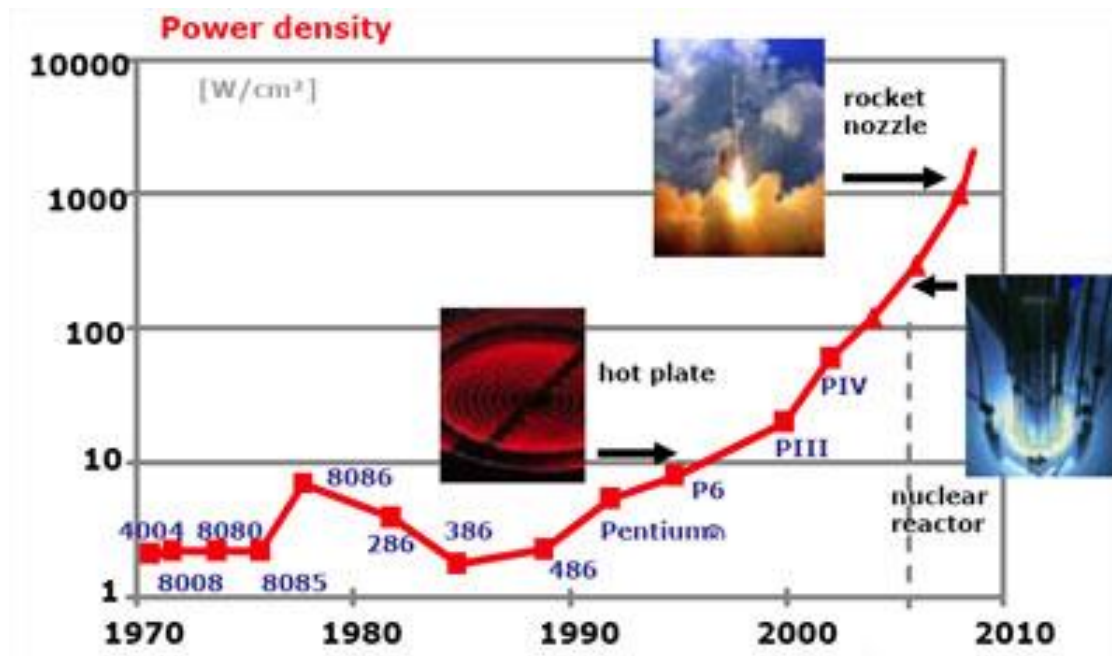
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Outline

- Motivation
- Problem Description
- Related Work
- Proposed Model
- Results
- Summary

Temperature – First Order Design Constraint



Heat Flux Trends over the Years

Temperature – First Order Design Constraint

Performance

Increase in Wire
delay

Reliability

Decrease in MTTF
Timing Errors

Thermal
Rundown

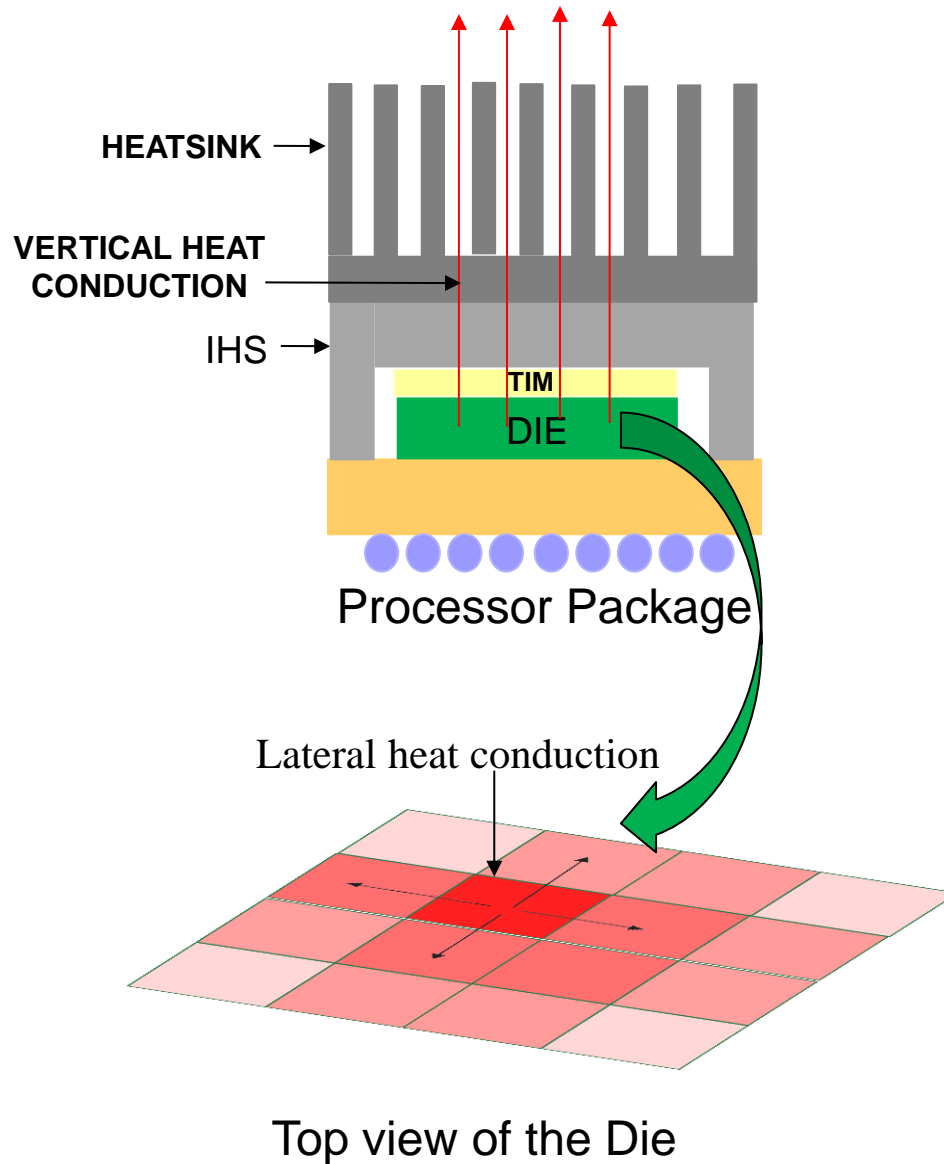
Temperature – Leakage
Feedback Loop

Temperature Estimation – Need and Importance

- Floorplanning and Placement
- Leakage convergence – **Slow Process**

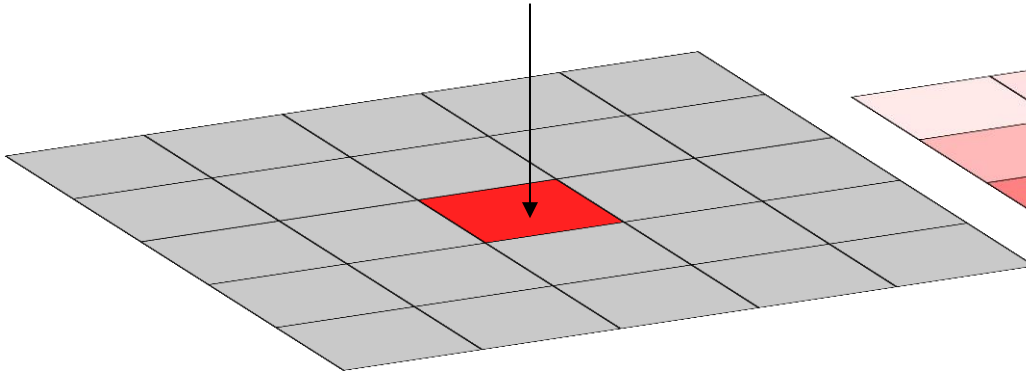


Heat Conduction in Microprocessors



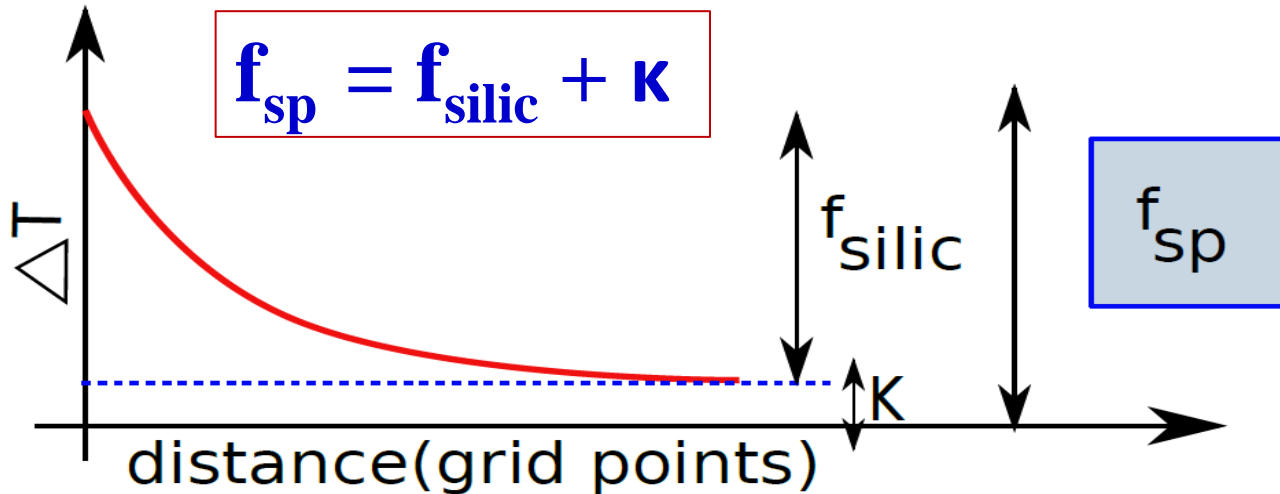
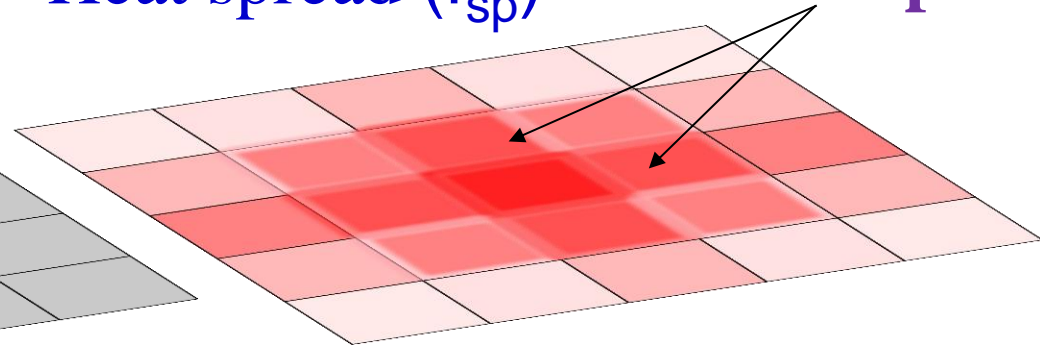
Temperature Distribution in a Chip

Point Source (1W)



Heat spread (f_{sp})

Isotropic



Relation between ΔT and radial distance (r)

Temperature Distribution in a Chip

- Fourier's heat equation –
$$\frac{\partial U}{\partial t} = \alpha_1 \nabla^2 U + \alpha_2 Q$$

U = Temperature Field, Q = Power Flux

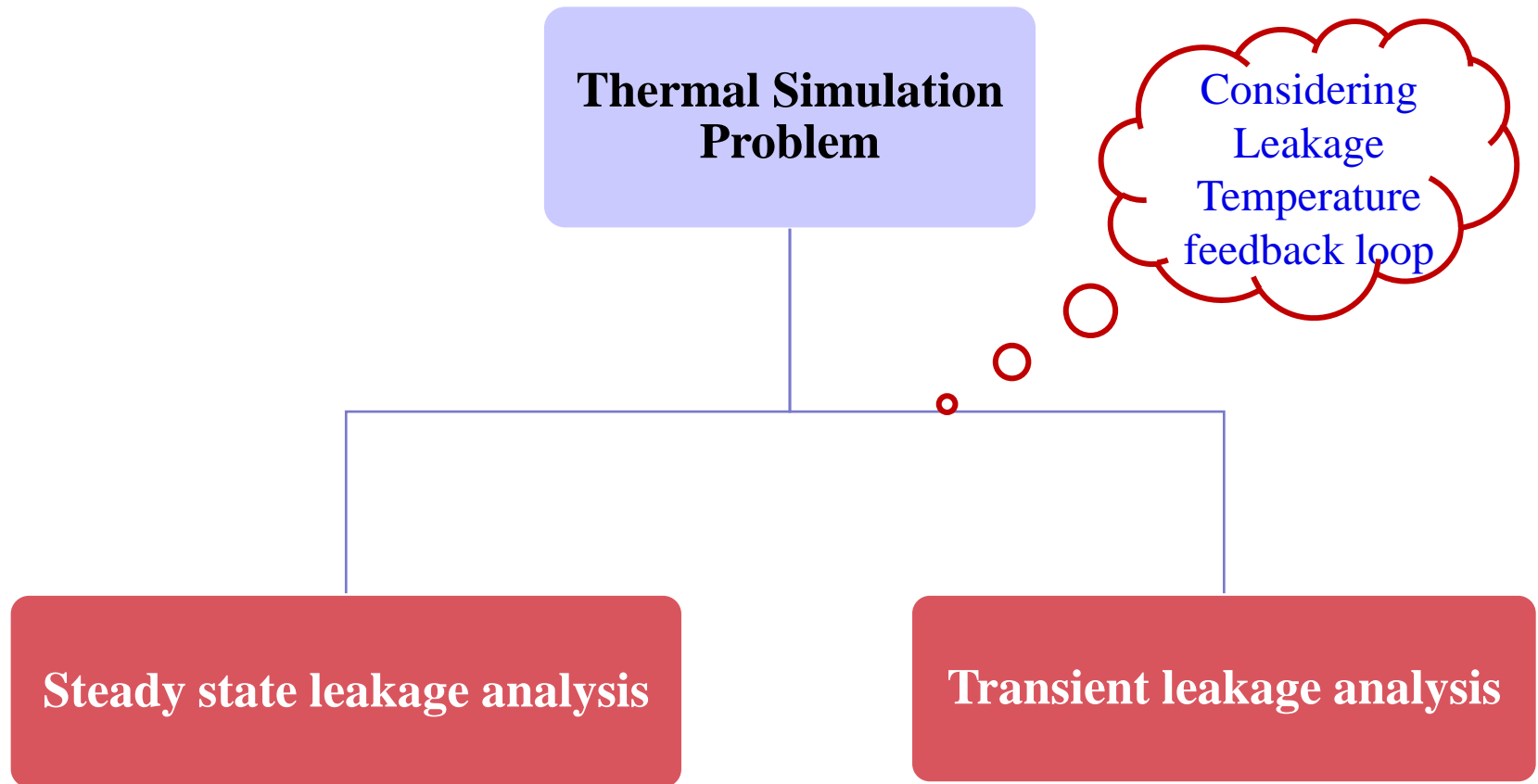
- Green's function (G) - **Impulse response** of an inhomogeneous differential equation defined on a domain

$$U(x' y' z') = \int G(x, y, z | x', y', z') Q(x' y' z') dx' dy' dz'$$

$$U = G \otimes Q$$

- Heat Spread function - **Green's function of the system**

Problem description





Problem description

To develop a faster and accurate temperature estimation tool

- Derive a transient and steady state Green's function of the chip

(Considering leakage-temperature feedback loop)

Related Work

Existing thermal simulators essentially use one of the following methods

- Finite element method
- Finite difference method
- Boundary element method
- Spectral based method

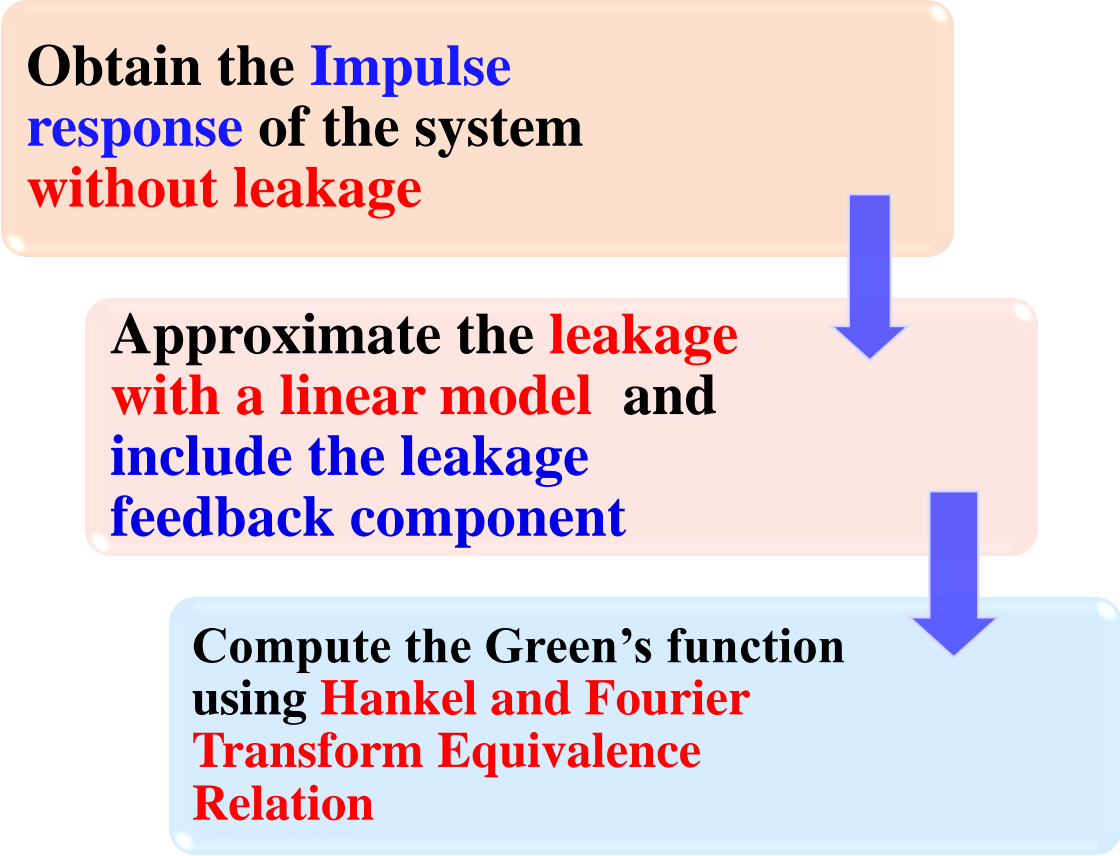
Krylov Subspace
Alternate Direction
Implicit
Adaptive Meshing
Multigrid methods

Related Work

- Hotspot (Skadron et al. ISCA'03)
 - Thermal electrical duality and FDM
- CONTILTS (Han et al. J.LPE'07)
 - Piecewise Constant Approximation of power trace
- Power Blurring (Park et al. SemiTherm'10)
 - Thermal mask convoluted with power density
distribution

Proposed Model

Obtain the **Impulse response** of the system **without leakage**



```
graph TD; A[Obtain the Impulse response of the system without leakage] --> B[Approximate the leakage with a linear model and include the leakage feedback component]; B --> C[Compute the Green's function using Hankel and Fourier Transform Equivalence Relation];
```

Approximate the **leakage with a linear model** and **include the leakage feedback component**

Compute the Green's function using **Hankel and Fourier Transform Equivalence Relation**

Benefits

- Traditionally **Impulse response is converted to Fourier transform** and inverse Fourier transform is used **to obtain the Green's function**

- **Fourier Transform (2D space) – Complexity : $O(N^2)$**

- Our Model uses **Hankel Transform (1D space) – Complexity: $O(N)$**

Assumptions

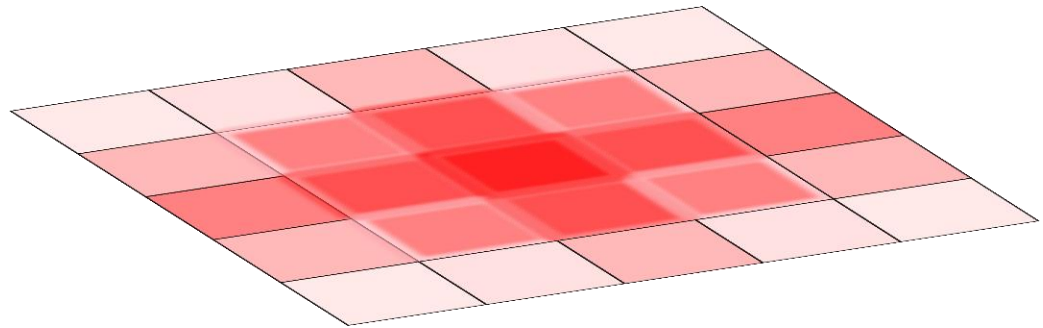
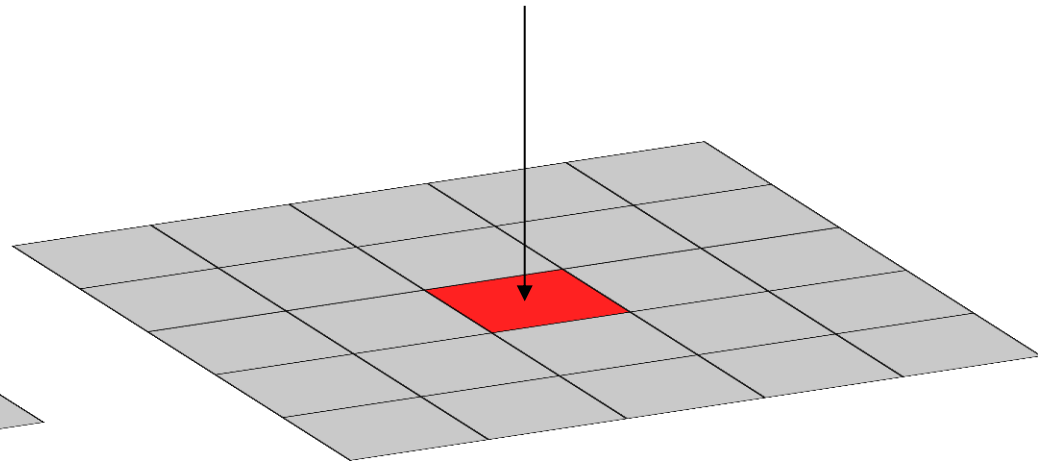
- **Die is very large
(theoretically infinite)**
- **f_{silic} is radially symmetric**
- **Heat sources are on the die
surface and we restrict our
computations to the top
surface of the die**
- **Leakage power increases
instantaneously**

Crux of our Technique

$$U_0 = T_{\text{ambient}}$$

$$P_{\text{leak}} = P_{\text{leak}0} \ \& \ P_{\text{dyn}} = 0$$

Unit Power source



$$U_p = T$$

$$P_{\text{leak}} = P_{\text{leak}} \ \& \ P_{\text{dyn}} = 1$$

Steady state Leakage Problem

$$Q = P_{\text{dyn}} + P_{\text{leak}} = \text{Total Power dissipation}$$

$$\Delta T = U = U_p - U_0 = \text{Change in Temperature Field}$$

$$U = G \otimes Q = (f_{\text{sp}}) \otimes (P_{\text{dyn}} + \beta U)$$

Linear Leakage
Approximation

$$\beta f_{\text{sp}} \otimes U = \text{Leakage Feedback component}$$

$$U = f_{\text{silic}} + \kappa + \beta f_{\text{silic}} \otimes U + \kappa_1$$

Fourier Hankel Equivalence

- 2D Fourier Transform $F(s,t)$

$$\frac{1}{2\pi} \iint_{-\infty}^{\infty} e^{-j(xs+yt)} dx dy$$

- Zero Order Hankel Transform $H(k)$

$$\int_0^{\infty} f(r) J_0(sr) r dr$$



f_{silic} is
radially
symmetric

Zero Order Hankel Transform is equivalent to
2D Fourier Transform of radially symmetric functions
in polar co-ordinates

Hankel Transformation

- $$H(U) = \frac{H(f_{silic}) + (\kappa + \kappa_1)H(1)}{1 - 2\pi\beta H(f_{silic})}$$

- Inverse Hankel = $H^{-1}H(U) = f_{leaksp}$



**Modified
Green's
function**

$$f_{leaksp} = f_{silic} + 2\pi\beta H^{-1}(H(f_{silic})^2) + \phi$$

Transient Leakage Problem

Here we start with

$$U = f_{sp} + \beta f_{sp} \otimes U - C f_{sp} \otimes \frac{\partial U}{\partial t}$$

- We follow similar steps and use **Leibnitz rule**
- **Boundary conditions :**
 - At $t = 0$, $H(U) = 0$
 - At $t = \infty$, $H(U) = H(f_{leaksp})$

Transient Leakage Problem

- Solving for t and applying boundary conditions

$$\mathcal{H}(U) = \mathcal{H}(f_{leaksp}) \times \left(1 - e^{-\frac{t}{f_{\alpha}(s)(\kappa\delta(s)/s + \mathcal{H}(f_{silic}))}}\right)$$

- Inverse Hankel transformation $\rightarrow f_{trans}(r,t)$

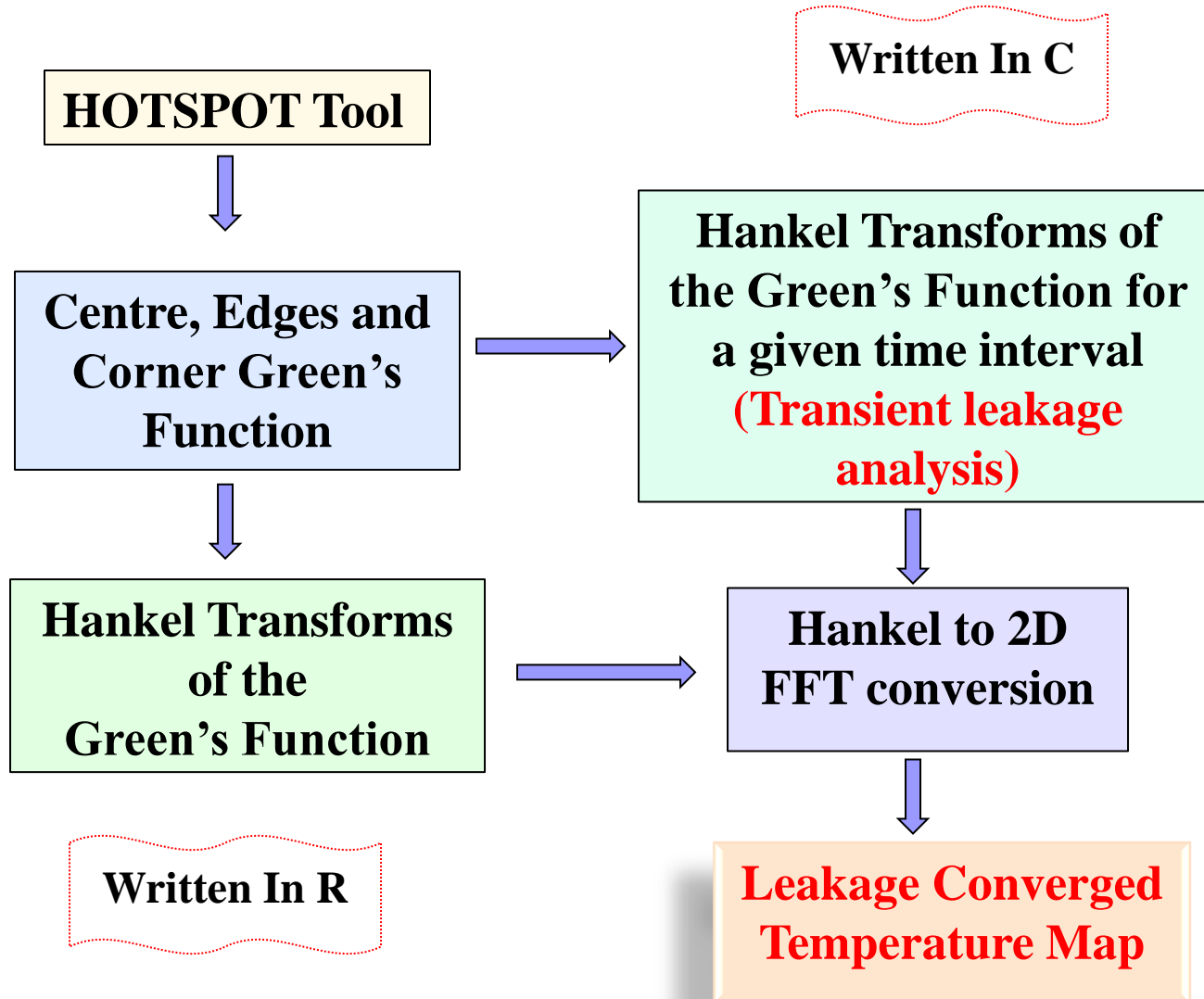
Effect of heating up the entire package

Transient temperature rise in the neighborhood

$$f_{trans}(r,t) = f_{leaksp}(r) - f_{inv}^{\epsilon}(r,t) - f_{inv}^{\infty}(r,t)$$

0
 ϵ

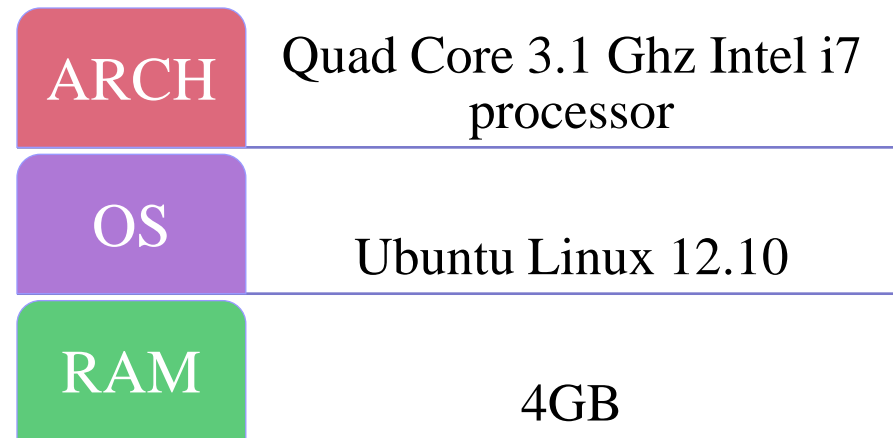
Experimental Setup



Experimental Configuration

PARAMETER	VALUE
Die Size	400 mm ²
Silicon Conductivity	130 W/m-K
Spreader Conductivity	370 W/m-K
Heat sink Conductivity	237 W/m-K
Convection Resistance	0.1 K/W
Spreader Thickness	3.5 mm
Heatsink Thickness	24.9 mm

Hotspot tool Configuration

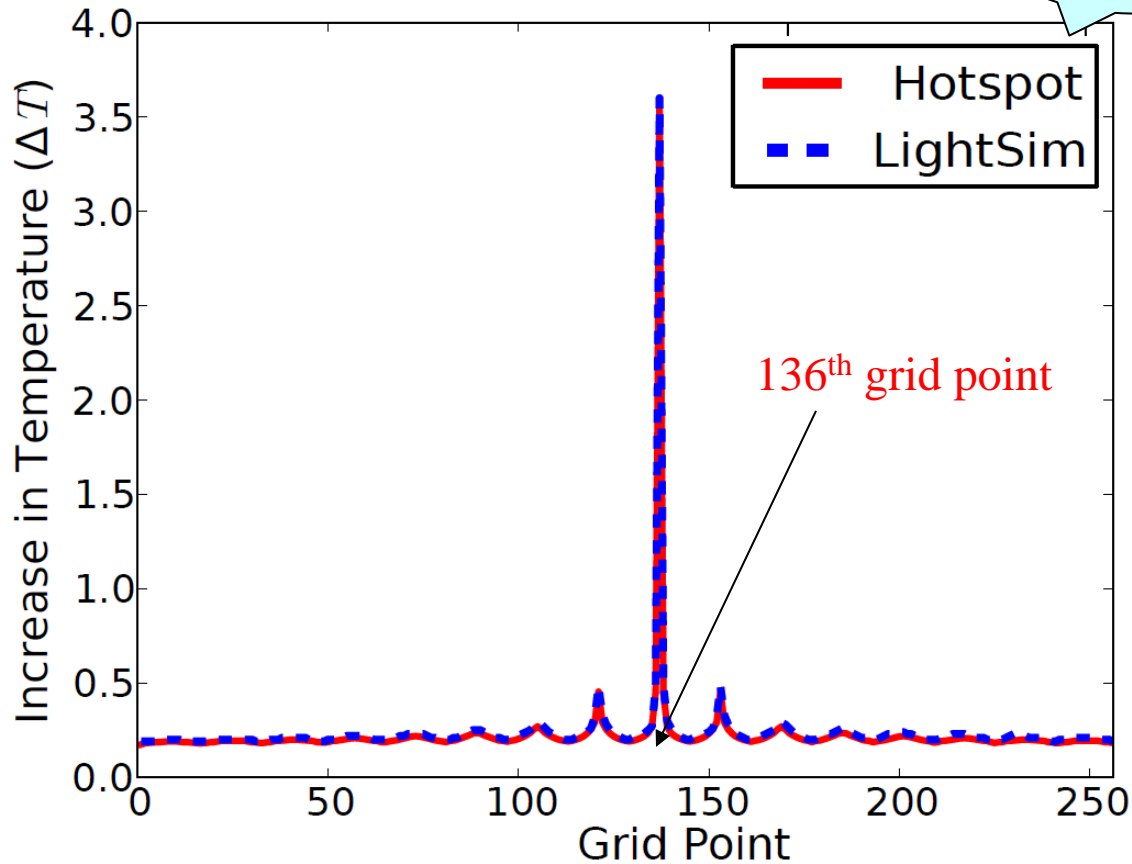


Experimental Environment

Results - Accuracy

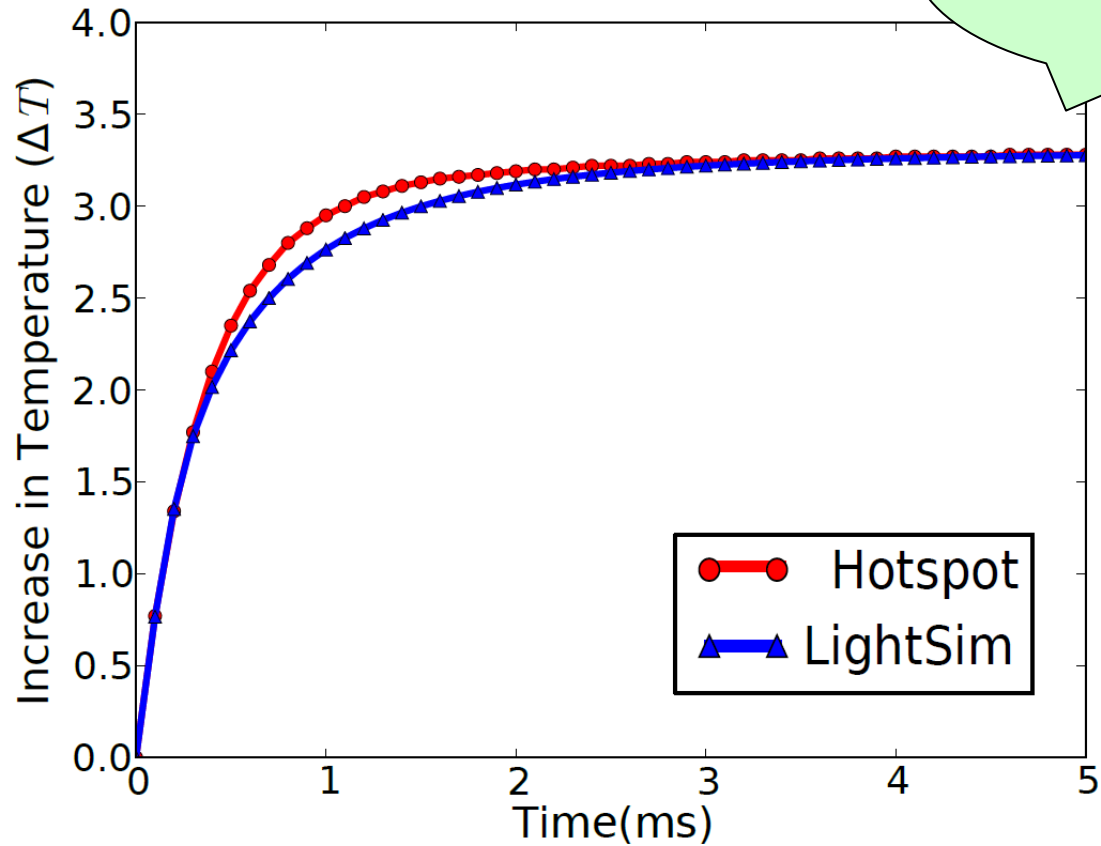
Steady state Leakage Green's function

Error is
< 2 %



Results – Accuracy

Transient Leakage Green's function



**Max Error is
4.5% (0.18°C)**

Results - Speed

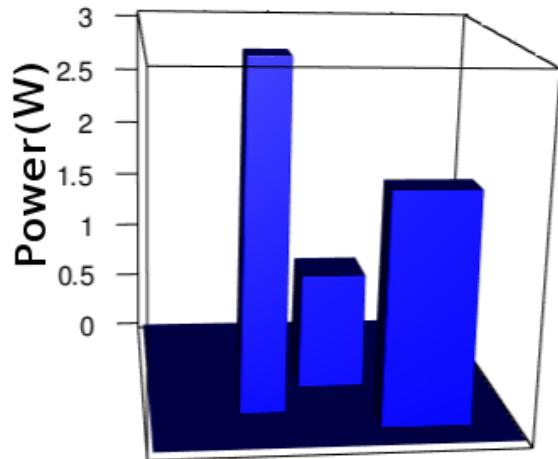
SIMULATOR	STEADY STATE LEAKAGE	TRANSIENT LEAKAGE
HOTSPOT 5.02	30.3 ms	45s
CONTILTS	25.2 ms	206.4 ms
Liu et. al.	39.3 ms	264.8 ms
PowerBlur	20.1 ms	58.2 ms
LightSim	8.7 ms	12.8 ms

3500 X

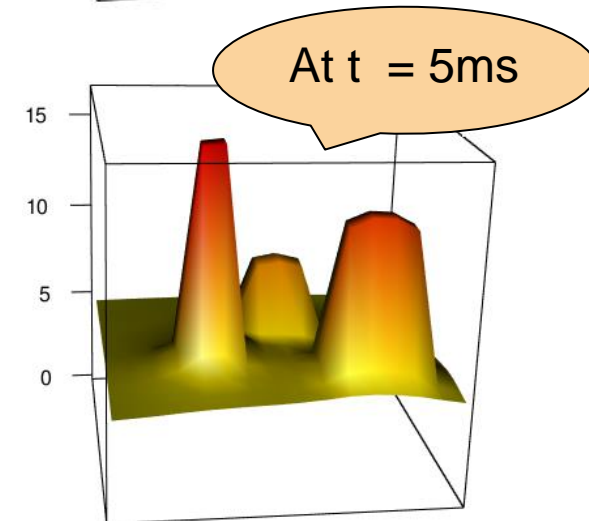
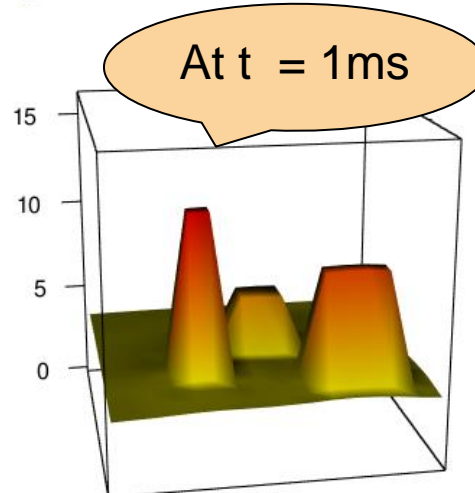
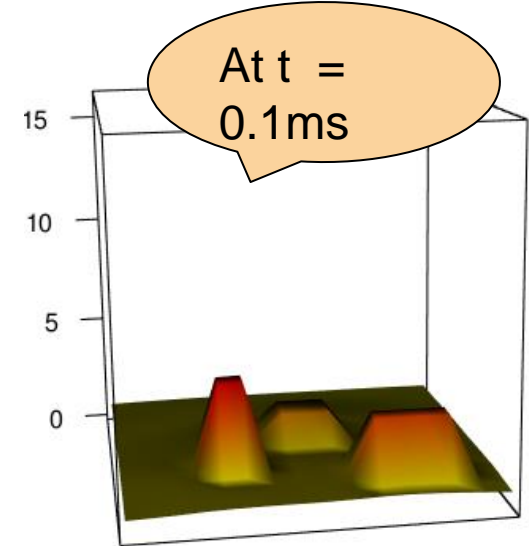
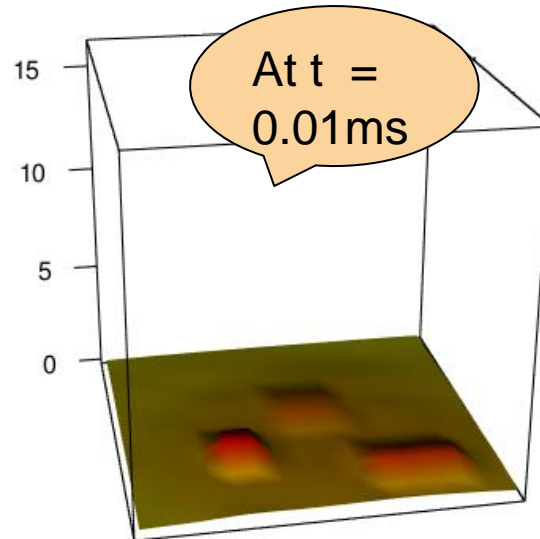
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Results – Sample Simulation

Sample Power Map



ΔT variation with TIME



Errors of different regions

Location	Error (%)	
	steady state	transient(at 2ms)
Center	0.6%	1%
Edge	1%	1.8%
Corner	1.8%	2.4%

Summary

- An **efficient Hankel transform based** thermal simulator has been developed
- Has a complexity of **$O(n \log(n))$** time
- Experimental results show that our model is fast and accurate.

Future Work:

- To develop more accurate models for edges and corners
- Comparison with ANSYS/COMSOL simulation

Figure Sources

1. <http://www.nanowerk.com> and Intel
2. <http://www.ausmotive.com>
3. www.facegfx.com



THANK YOU !!