

Surfliner: Approaching Distortionless Light-Speed Wireline Communication

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Outline

- Motivation
- Previous Work
- Surfliner
 - Overview
 - Theory
 - Implementation
 - Simulation Results
- Applications
- Conclusions



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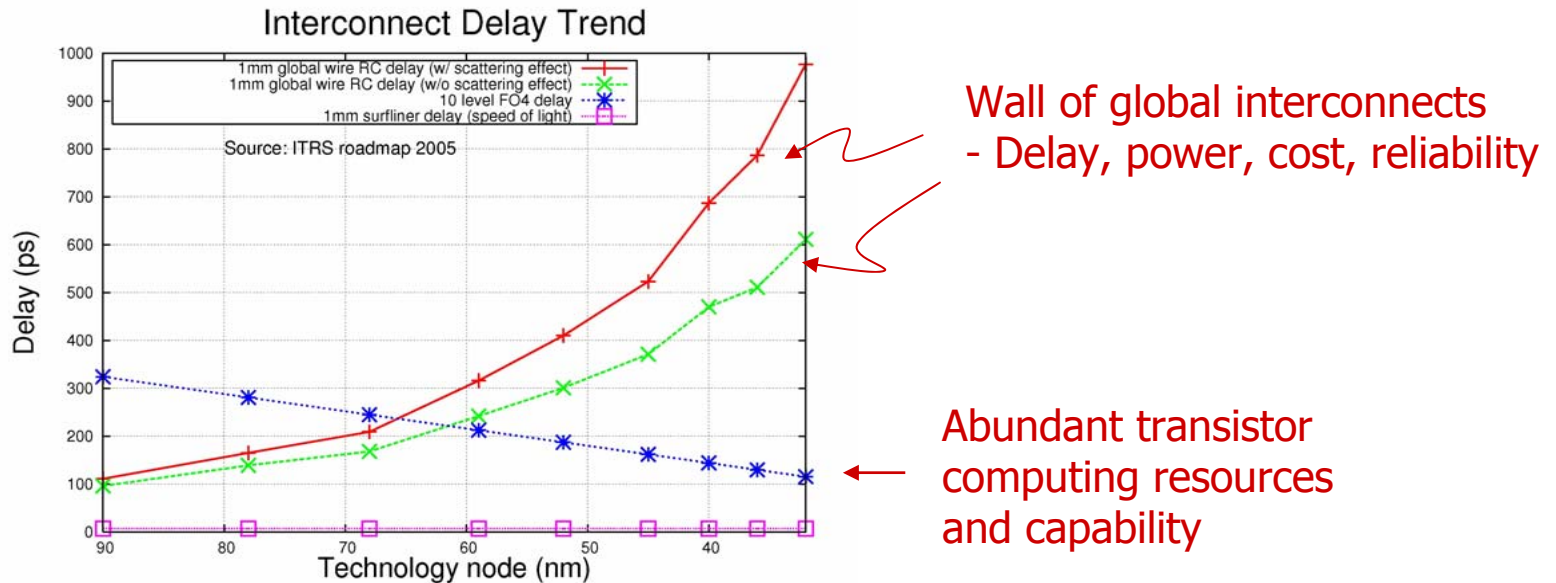
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Motivation — On-chip Perspective

- On-chip global interconnect trend



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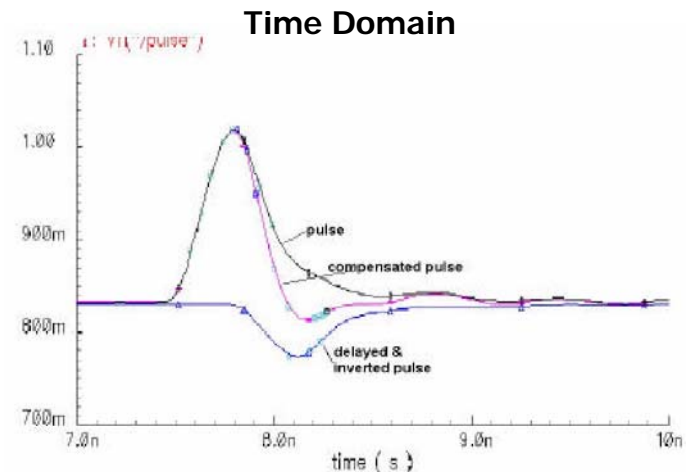
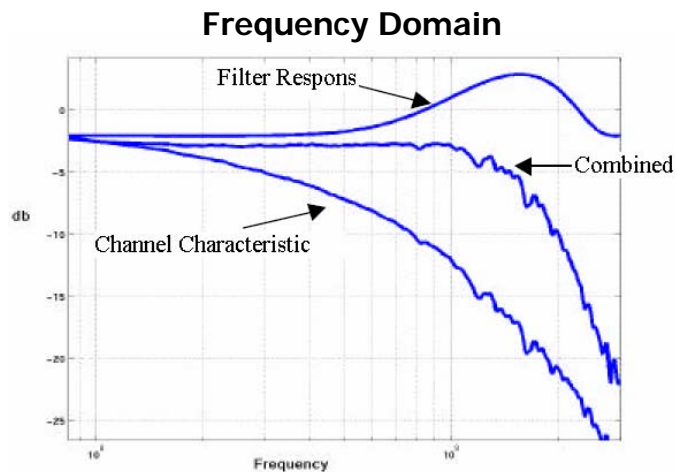
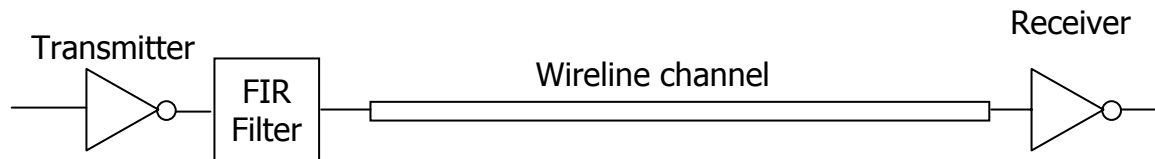
Previous Work

- Existing on-chip serial link signaling schemes
 - Pre-emphasis and equalization (W. Dally, '98)
 - Clocked discharging (Horowitz, ISVLSI'03)
 - Frequency modulation (Wong, JSSC'03; Jose, ISVLSI'05)
 - Non-linear transmission line (Hajimiri, JSSC'05, E. C. Kan, CICC'05)
 - Resistive termination (Hashimoto, EPEP'04, Tsuchiya, CICC'04, Flynn, ICCAD'05, CICC'05)



Pre-emphasis

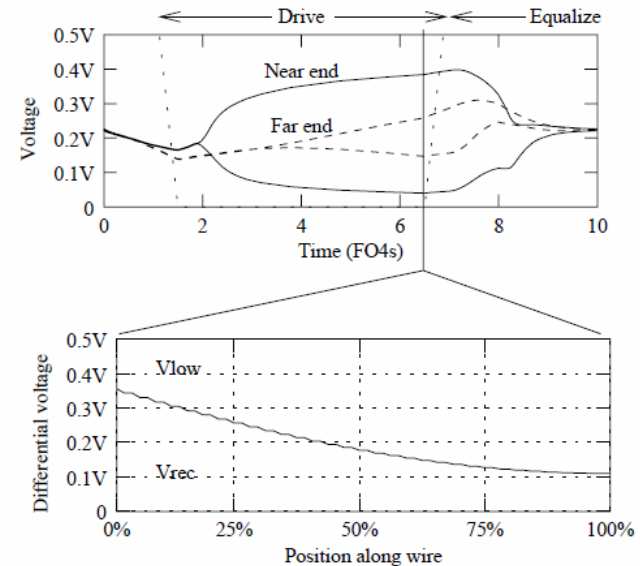
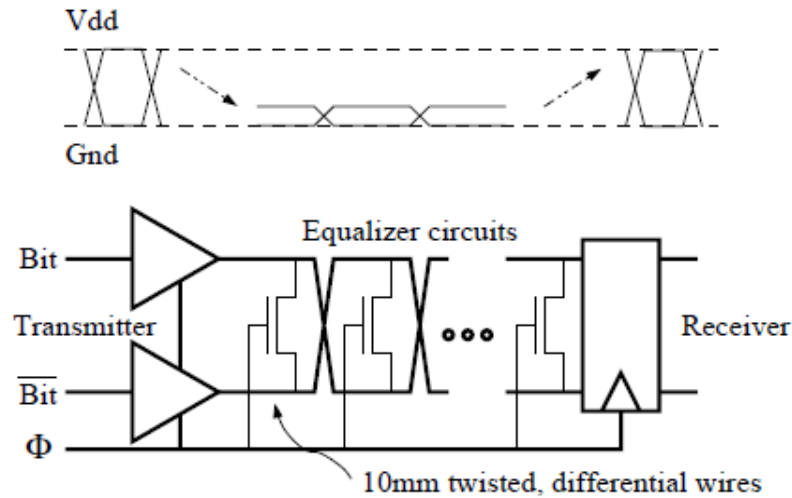
- A high-pass filter at the transmitter side to compensate the channel characteristic



Pictures courtesy of Johnny Zhang and Zhi Wang, "White paper on transmit pre-emphasis and receive equalization"



Clocked Charge Recycling



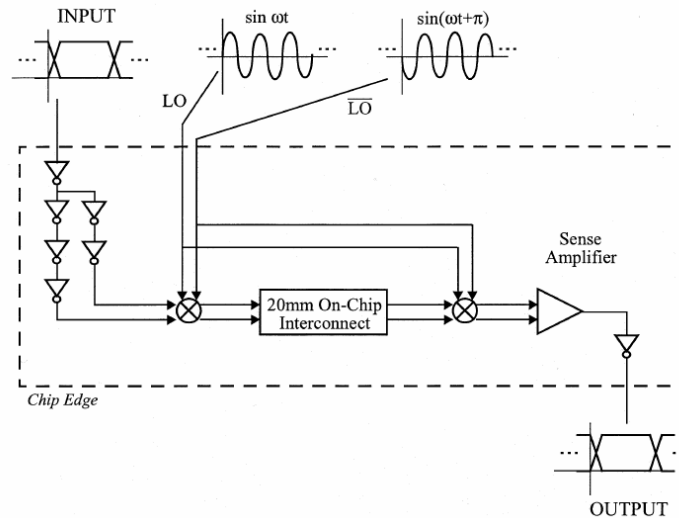
- Essentially time-domain equalization directly implemented on the wire



Frequency Modulation

- Modulate the data to high-frequency (LC region) to achieve speed-of-light, low distortion transmission

Richard T. Chang, Simon Wong, JSSC '03

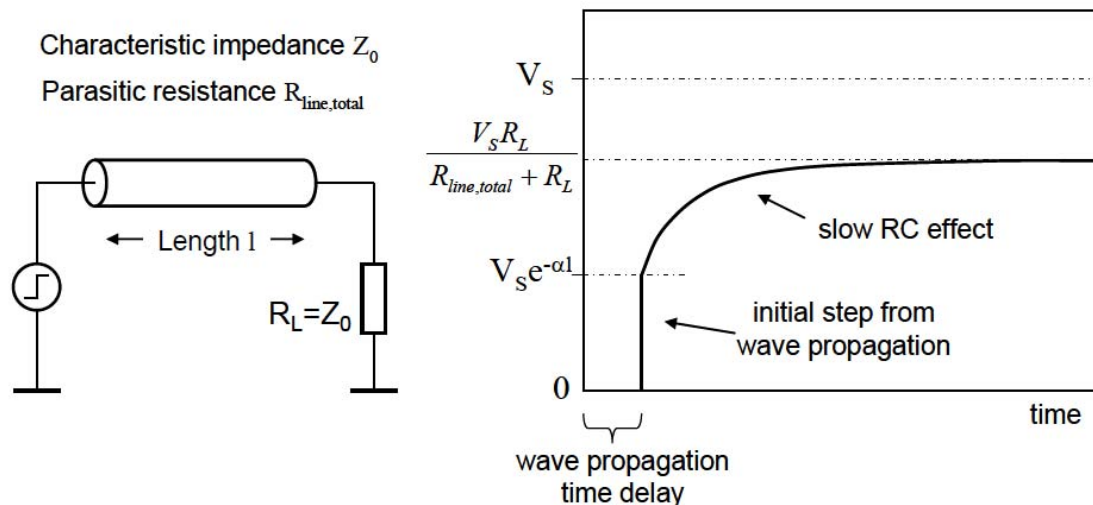


- Use RZ bit piece instead of NRZ, and reduce the duty cycle to push more frequency content to the higher spectrum (Jose et al., ISVLSI '05)



Resistive Termination

- Use resistive termination to cut the slow RC tail




Michael Flynn, ICCAD '05

- Tsuchiya et al. developed an analytical model for eye opening with resistive termination (CICC '05)



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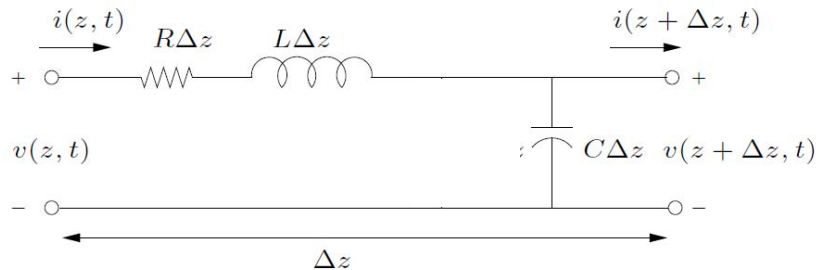
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Surfliner — Overview

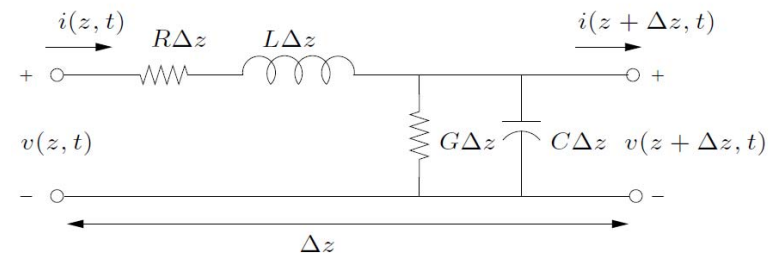
- Single-ended case

Typical on-chip Transmission Line



- negligible leakage conductance
- Frequency dependent phase velocity (speed) and attenuation

Distortionless Transmission Line



- **Intentionally** make leakage conductance satisfy $R/G=L/C$
- Frequency response becomes flat from DC mode to Giga Hz



Telegrapher's Equations

- Telegrapher's equations

$$\begin{aligned}\frac{\partial V(z,t)}{\partial z} &= -RI(z,t) - L\frac{\partial I(z,t)}{\partial t} \\ \frac{\partial I(z,t)}{\partial z} &= -GV(z,t) - C\frac{\partial V(z,t)}{\partial t}\end{aligned}$$

- Wave Propagation

$$V(z) = V_0 e^{-\alpha z - j\beta z} \quad I(z) = V(z)/Z_0$$

- Propagation Constant

$$\gamma = \sqrt{(R + j\omega L)(G + j\omega C)} = \alpha + j\beta$$

- Characteristic Impedance

$$Z_0 = \sqrt{\frac{R + j\omega L}{G + j\omega C}}$$

- α and $v = \omega/\beta$ correspond to attenuation and phase velocity. Both are **frequency dependent** in general.



On-Chip Wires

- RC Region $\omega L \ll R, G \approx 0$

$$\begin{aligned}\gamma = \alpha + j\beta &= \sqrt{(R + j\omega L)(G + j\omega C)} \\ &\approx \sqrt{j\omega RC} \\ &= \sqrt{\frac{\omega RC}{2}} + j\sqrt{\frac{\omega RC}{2}}\end{aligned}$$

$$Z = \sqrt{\frac{R}{j\omega C}} \quad v = \sqrt{\frac{2\omega}{RC}}$$

Typical on-chip wire: $R = 2 \Omega/\mu\text{m}$ ($A=0.01 \mu\text{m}^2$)
 $L = 0.3 \text{ pH}/\mu\text{m}$, $C = 0.2 \text{ fF}/\mu\text{m}$
 $R/L = 0.67\text{E}+12$



LC Region

- If $\omega L \gg R, G \approx 0$

$$\begin{aligned}\gamma = \alpha + j\beta &= \sqrt{(R + j\omega L)(G + j\omega C)} \\ &= \sqrt{(R + j\omega L)j\omega C} \\ &= \frac{R}{2\sqrt{L/C}} + j\omega\sqrt{LC}\end{aligned}$$

$$Z_0 = \sqrt{\frac{L}{C}} \quad \alpha = \frac{R}{2Z_0} \quad v = \frac{1}{\sqrt{LC}}$$

This is the premise of the frequency modulation approaches



Surfliner — Theory

- Distortionless transmission line

$$\text{If } \frac{R}{G} = \frac{L}{C}$$

$$\begin{aligned} \gamma = \alpha + j\beta &= \sqrt{(R + j\omega L)(G + j\omega C)} \\ &= \frac{R}{\sqrt{L/C}} + j\omega\sqrt{LC} \end{aligned}$$

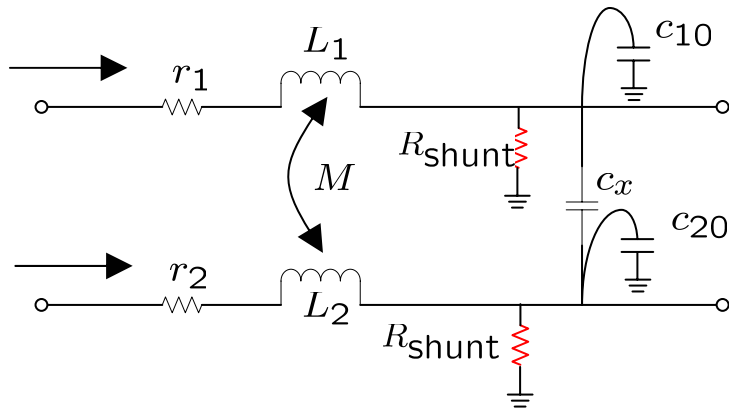
$$Z_0 = \sqrt{\frac{L}{C}} \quad \alpha = \frac{R}{Z_0} \quad \boxed{v = \frac{1}{\sqrt{LC}}}$$

Both attenuation and phase velocity become frequency independent

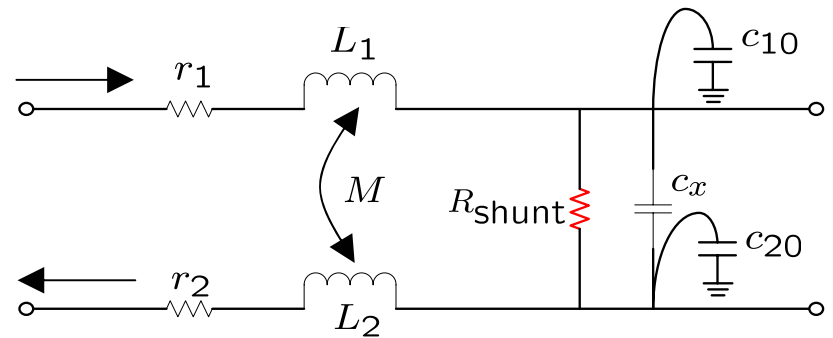


Surfliner — Differential Case

Common Mode – Current flowing in the same direction



Differential Mode – Current flowing in the opposite direction



Shunt between each line to ground

$$R_{\text{shunt}} = Z_{\text{even}}^2 / R_{\text{series}}$$

$$Z_{\text{even}} = \frac{(1 + M)L_1}{C_{10}}$$

Shunt between the two lines

$$R_{\text{shunt}} = 2Z_{\text{odd}}^2 / R_{\text{series}}$$

$$Z_{\text{odd}} = \frac{(1 - M)L_1}{C_{10} + 2C_x}$$



Surfliner — Implementation

- Evenly add shunt resistors between the signal line and the ground



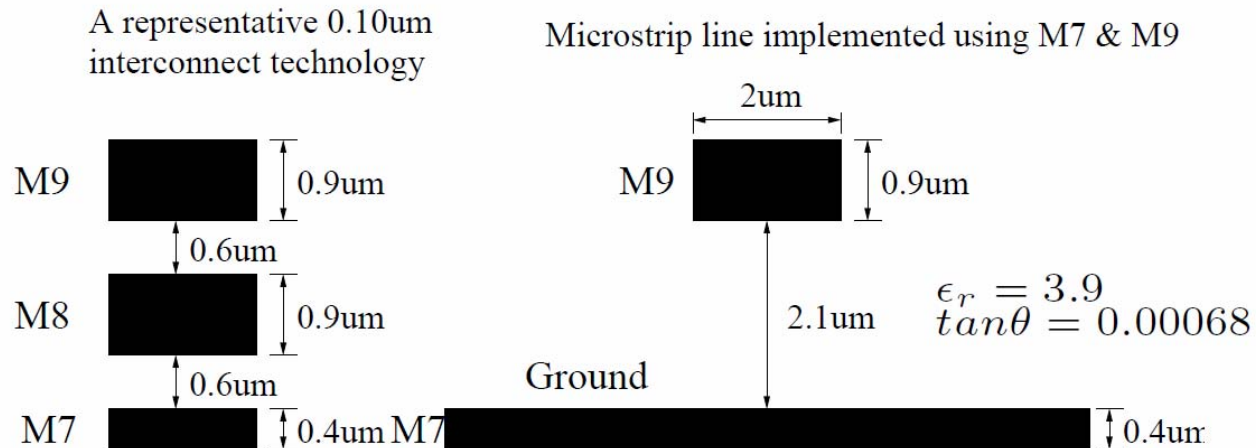
- Non-ideality

Ideal Surfliner	In Practical	Implication
Homogeneous and distributive	Discrete	What's the optimal spacing? Are the shunt resistors realizable?
RLGC are frequency independent	RLGC vary over frequency	What's the optimal frequency to do the matching?



Surfliner — Simulation

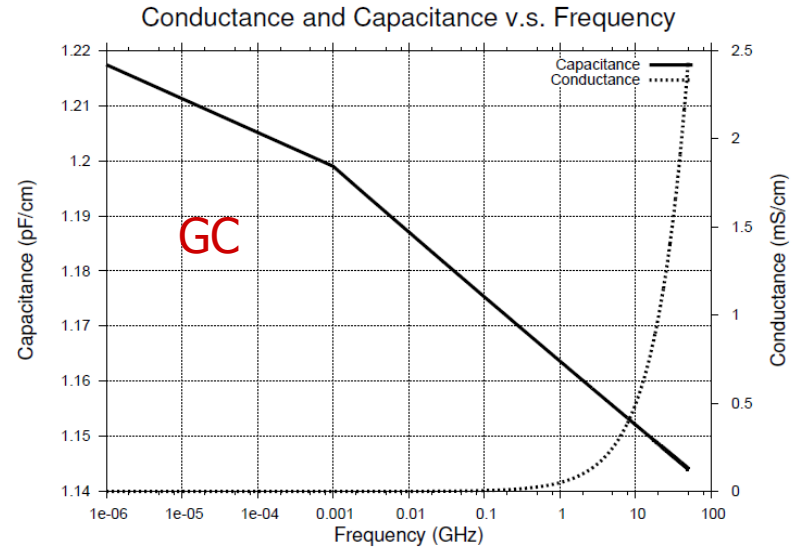
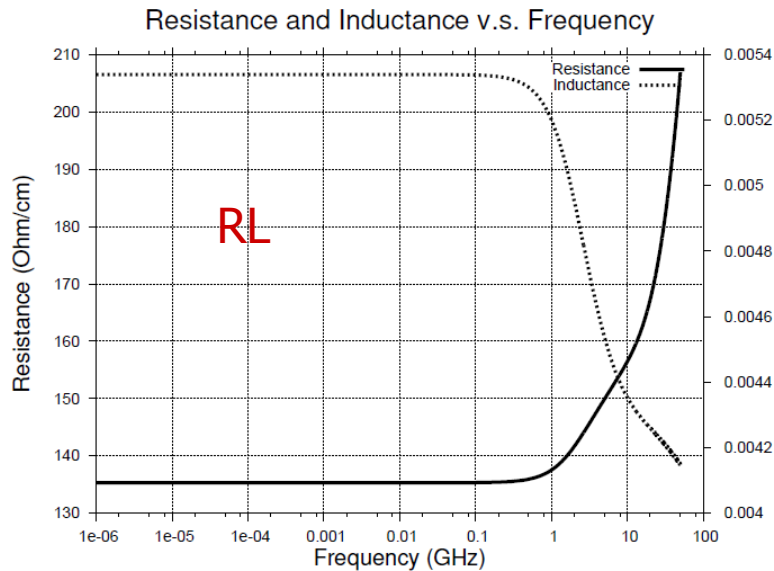
- On-chip single-ended stripline, 10 mm



Draw not to scale



RLGC parameters



$$Z_0 = 54.7 \, \Omega, \text{ speed} = 65.87 \, \text{ps/cm}$$

- Match at DC
 - Boost up low frequency traveling speed
 - Balance low frequency attenuation and high frequency attenuation

$$R_{1\text{MHz}} = 135.4 \, \Omega/\text{cm}, L_{1\text{MHz}} = 5.34\text{E-}3 \, \mu\text{H}/\text{cm}, C_{1\text{MHz}} = 1.217 \, \text{pF}/\text{cm}$$

$$G = R_{1\text{MHz}} C_{1\text{MHz}} / L_{1\text{MHz}} = 32.41 \, \Omega/\text{cm}$$



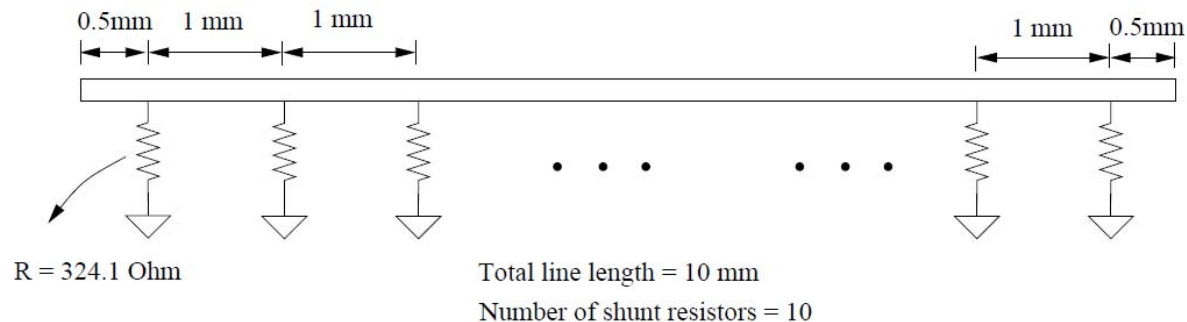
Shunt Resistor Spacing

- Assuming insert N shunt resistors

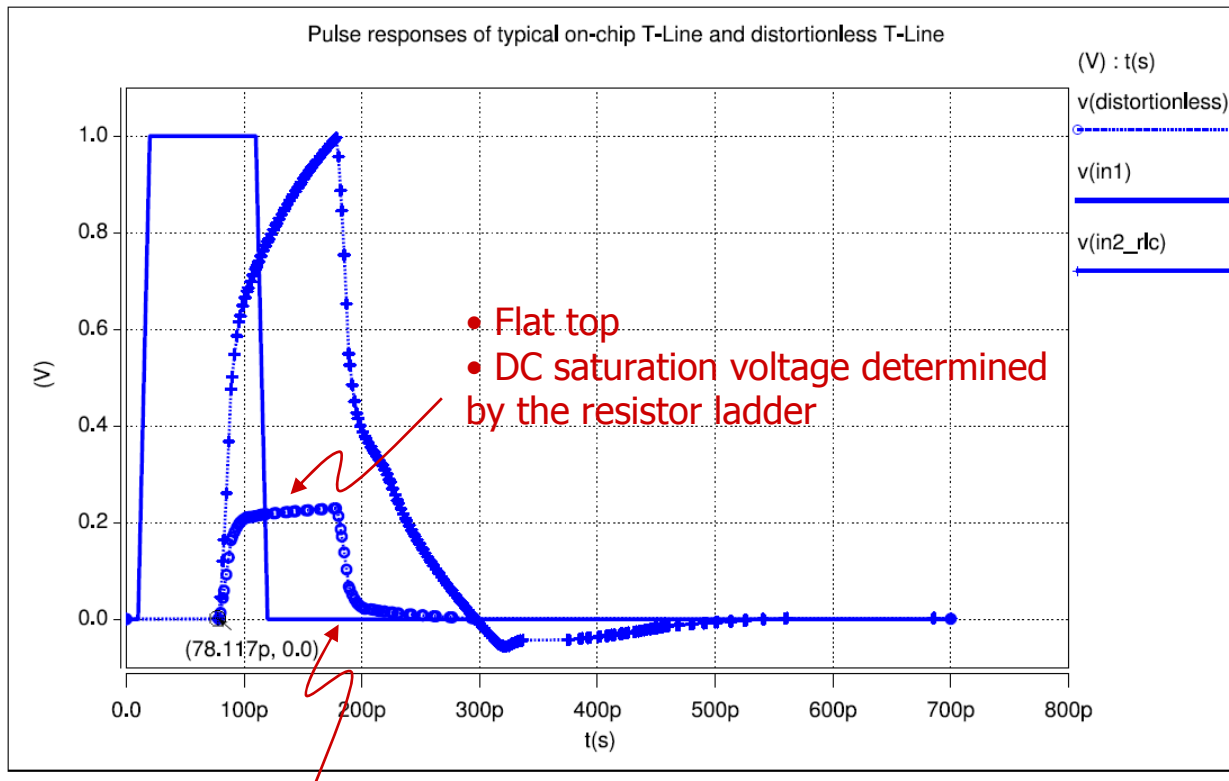
$$R_{\text{single}} = N \cdot R_{\text{shunt, total}}$$

- Optimal spacing depends on the target data rate

$$L_{\text{crit}} = \frac{c}{\sqrt{\epsilon_r}} \cdot t_r$$



Pulse Response

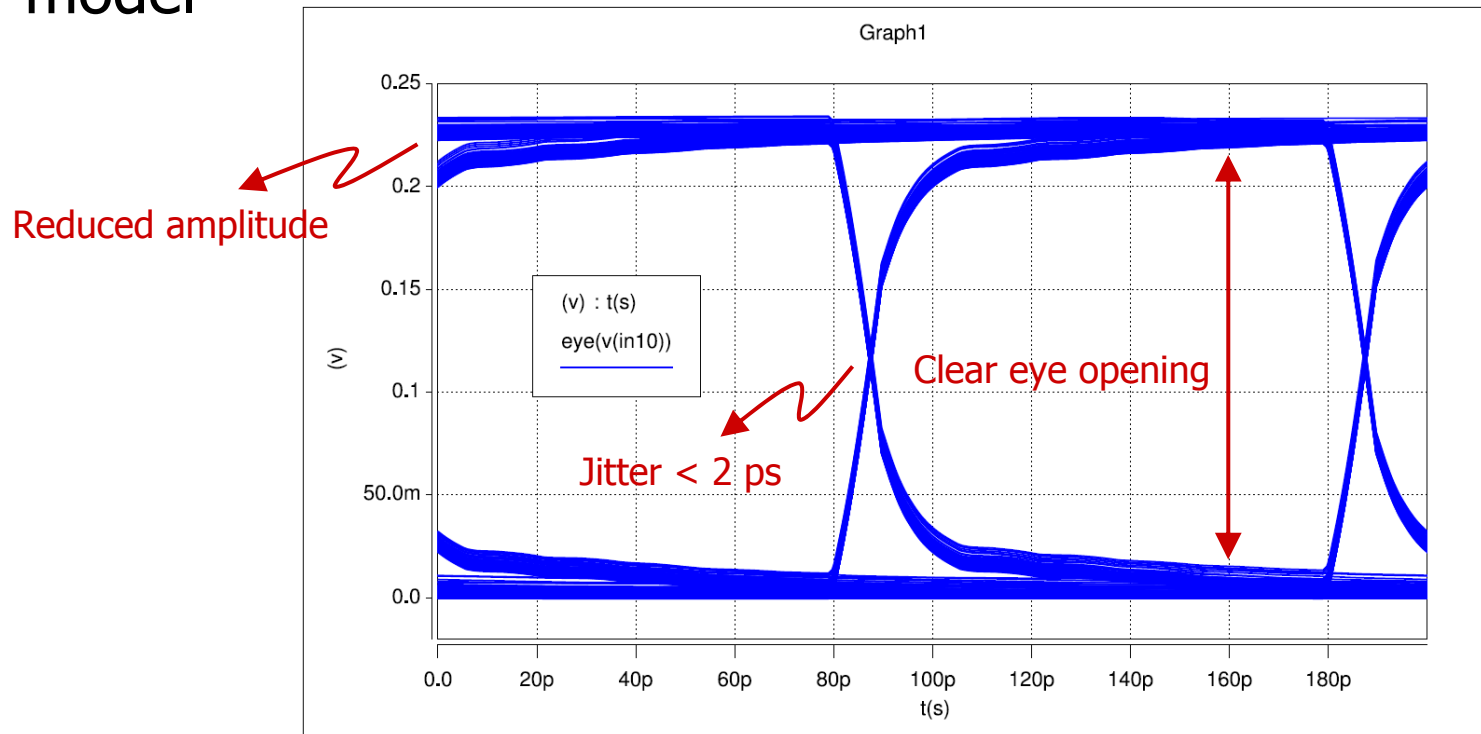


- ISI effect greatly suppressed

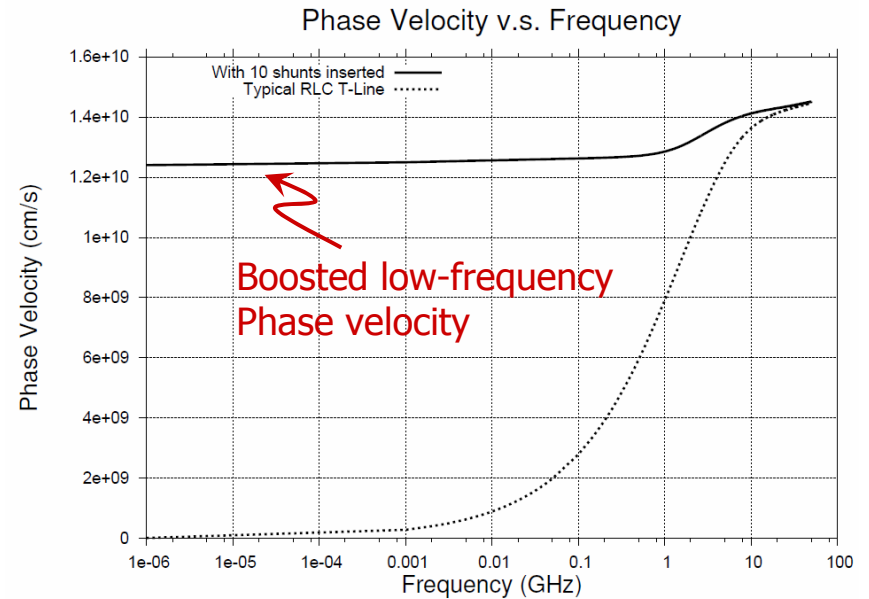
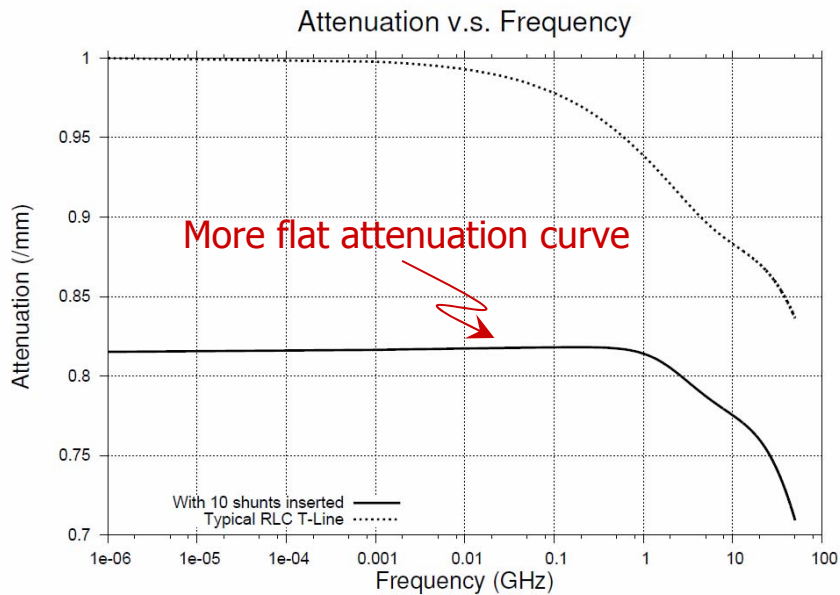


Eye Diagram

- 1000 bit PRBS at 10Gbps
- Simulated in Hspice using W-element + tabular RLGC model



A Frequency Domain Perspective



Power Consumption

- Would static power consumption through shunt resistors kill Surfliner?
 - Measured P_{avg}
 - Calculate $E_{bit} = P_{avg} * T_{cycle}$

Bit Rate (Gbps)	5	10	20	40
P_{avg} (mW)	2.5624	2.5754	2.6544	2.7612
E_{bit} (pJ)	0.5125	0.2575	0.1327	0.0690



Conclusions

- Demonstrated feasibility and superiority of Surfliner scheme
- Test chip fabrication (joint with Osaka)
 - Waiting for testing results
- Future work
 - More applications: clock tree, etc.
 - Model data-dependent jitter
 - Incorporate transmitter/receiver design



The End

Thank you!

