Phone-nomenon: A System-Level Thermal Simulator for Handheld Devices

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2019 Asia and South Pacific Design Automation Conference

Outline

- Motivation
- Thermal model for handheld devices
 - Modeling for internal heat transfer effects
 - Modeling for boundary conditions
- Overall thermal simulation flow
- Experimental results
- Conclusions



Motivation (1/3)

- The sales of handheld devices have surpassed that of PCs in 2011
- Relative high power consumption on small-form factor



- Why consider thermal issues on smartphones
 - Higher performance on application processors (AP) (A4~A12, Exynos 4~9 Series, Snapdragon 200~850 Series, Helio P10~90)
 - Cooling techniques
 - PC: active cooling (fans, forced convection)
 - Smartphone: passive cooling (free air, free/nature convection)



Motivation (2/3)

• When device executes heavy operations



Motivation (3/3)





Contributions

- Phone-nomenon considers the heat transfer mechanism around handheld devices
 - Internal heat transfer
 - External heat transfer
- Phone-nomenon builds an iterative framework thermal simulation flow
- Phone-nomenon can achieve two and three orders of magnitude speedup with 3.58% maximum error and 1.72°C difference for steady-state and transient simulations



Handheld Device Architecture Thermal Test Vehicle



Heat Transfer Mechanisms for Handheld Devices

- Internal heat transfer
 - Conduction, convection, radiation
- External heat transfer
 - Convection, radiation





Internal Heat Transfer Conduction for Solid Structure

Circuit simulation Thermal simulation

Voltage (V) $\leftarrow \rightarrow$ Temperature (T) Current (I) $\leftarrow \rightarrow$ Power (P)



- By using finite difference method, the heat transfer governing equation for conduction $\Rightarrow C \frac{dT}{dt} + GT = P$ in matrix form (*C*: heat capacitance, *G*: thermal conductance)
- By LU factorization and backward Euler on the time differential part, the temperature *T* can be solved



Internal Heat Transfer Why Considering Conduction and Radiation for Air



The thermal effect of internal air in the smartphone. All results are obtained by Icepak



Internal Heat Transfer Conduction and Nature Convection for Air

- Conduction for air
 - The thermal conductivity of an air block is temperature dependent [1]
 - $\kappa_{air-cond} = -4.66 \cdot 10^{-3} + 1.68 \cdot 10^{-3} T_{air,K} 3.73 \cdot 10^{-7} T_{air,K}^2 + 6.94 \cdot 10^{-10} T_{air,K}^3 6.13 \cdot 10^{-13} T_{air,K}^4 + 1.97 \cdot 10^{-16} T_{air,K}^5$, where $T_{air,K} = T_{air} + 273.15$ is the air temperature in Kelvin.
 - Since $\kappa_{air-cond}$ for 80°C is 14% more than 25°C, we apply above equation into our model
- Nature convection for air
 - Rayleigh number (Ra) which is described as nature convection
 - *Ra* is much less than 1708 in most smartphones and scenarios, therefore no need to consider this effect



Internal Heat Transfer Thermal Radiation for Air

- We develop a thermal resistive network to consider the thermal radiation
- Heat flux between plates $- q_{ii} = \sigma F_{ii} A_i |T_i^4 - T_i^4|$
- Thermal equilibrium equation $-q_{ij} = g_{ij} |T_{i,K} - T_{j,K}| \text{ (i.e. } q = g\Delta T)$



• Air effective thermal conductivity (ETC) for radiation

$$-g_{ij} = \frac{F_{ij}A_i\sigma(T_i^4 - T_j^4)}{(T_i - T_j)}$$

 $-\kappa_{air-rad}$

• By combination of series and parallel circuits



External Heat Transfer (B.C.) Why Considering Conduction and Radiation for Air



Chip temperature versus effective HTCs. The power values of SoC and PMIC are 1.8W and 1.0W, respectively.





The influence of external thermal radiation effect for five test cases.





External Heat Transfer (B.C.) Nature Convection [2]

- Effective HTCs (convection) between covers and air
- For four vertical sides (S1~S4): $Nu = 0.68 + \frac{0.67Ra^{1/4}}{(1+(0.492/Pr)^{9/16})^{4/9}}$
- For top side (T1): $Nu = 0.54Ra^{1/4}$
- For bottom side (B1): $Nu = 0.27Ra^{1/4}$

• Effective HTCs:
$$h_{b,conv} = \frac{k_{air}}{L} N u$$





External Heat Transfer (B.C.) Thermal Radiation

- Energy released by the oscillations of electrons in matter (electromagnetic wave emits)
- Subsequent transport does not require any presence of any matter
- Effective HTCs (radiation) between covers and air
- For each side (S1~S4, T1 and B1) Effective HTCs $h_{b,rad} = \alpha e \left(T_{b,K} + T_{\infty,K} \right) \left(T_{b,K}^{2} + T_{\infty,K}^{2} \right) [2]$

 α is Stefan Boltzmann constant : 5.673 * $10^{-8}Wm^{-2}K^{-4}$ e is emissivity : 0.72~0.9



Internal/External Heat Transfer Summary

- Combine convection and radiation for inside air block ETCs: $k_{air}(T_{b,K}) = \kappa_{air-cond} + \kappa_{air-rad}$
- Combine convection and radiation on the boundaries Effective HTCs: $h_b(T_{b,K}) = h_{b,conv} + h_{b,rad}$



Steady-State Thermal Simulation Flow





Transient Thermal Simulation Flow





Test Cases for Steady-State Simulations









Steady-State Results (1/2)

Measurement		Icepak		Phone-nomenon					
Temperature (°C)		Temperature (°C)		Temperature (°C)		¢Error (%)			
						Measurement		Icepak	
SoC	PMIC	SoC	PMIC	SoC	PMIC	SoC	PMIC	SoC	PMIC
50.2	NA	51.25	38.38	51.34	38.19	4.52	NA	1.04	3.58
NA	55.0	32.01	56.31	31.91	57.18	NA	7.27	2.02	2.33
69.2	81.1	72.22	86.72	72.26	87.63	6.92	11.64	1.18	0.46
80.3	104.3	82.90	107.89	83.61	108.94	4.18	5.85	1.76	0.31
78.6	75.6	80.86	79.98	81.94	80.78	6.23	10.24	1.49	0.75
	Measu Tempe (° SoC 50.2 NA 69.2 80.3	MeasumentTemperature de la colspane de	MeasurementIceTemperature ($^{\circ}$ Temper ($^{\circ}$ SoCPMICSoC50.2NA51.25NA55.032.0169.281.172.2280.3104.382.9078.675.680.86	MeasurementIce→kTempy-ture ()Tempy-ture ()SoCPMICSoCSoCPMICSoCSo2NAS125So3S530S125So4S550S201So5S1201S631So3104.3S2301So3104.3S036So3S55.6S036	Measurement Ice μ Ice Ice	Measurement Icerret Icerret Icerret Tempert R^{2} R^{2} R^{2} R^{2} Soc PMIC Soc PMIC Soc PMIC 50.2 PMA 51.25 38.38 51.34 38.19 NA 55.0 32.01 56.31 31.91 57.18 69.2 81.1 72.22 86.72 72.26 87.63 80.3 104.3 82.90 107.89 83.61 108.94 78.6 75.6 80.86 79.98 81.94 80.78	Measurement Iceument Temperature ($^{\circ}$) Temperature ($^{\circ}$) Temperature ($^{\circ}$) Temperature ($^{\circ}$) Iceument Temperature ($^{\circ}$) Temperature ($^{\circ}$) <thttemperature (<math="">^{\circ}) Tempera</thttemperature>	MeasurementIceurst Temperature PMICTemperature Temperature PMICTemperature PMICIceurst PMICSoCPMICSoCPMICSoCPMICSoCPMICSoCPMICSoCPMICSoCPMICSoCPMICSoCPMICSoCSoCSoCSoCPMICSoCSoCPMICSoCSoCSoCSoCPMICSoC<	MeasureIce Iee

♦ Error at the middle point of die

Error < 11.64%

Error < 3.58%



Steady-State Results (2/2)



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Test Cases for Transient Simulations



Periodic-1 (total time): [10sec (on) +10sec (off)]*5

Periodic-2 (total time): [8.4sec (on) +8.4sec (off)]*5

Periodic workload	SoC Power (W)	PMIC Power (W)	4	I.	T	1	-TTV -TTV2
P1	3.000	0.000	2)3				
P2	0.000	1.160	od 1-				
	•	-					P 1

0

20

60

40

Time (sec)

80



100

Transient Results (1/2)

	Icepak	Phone-nomenon						
Case	Runtime	Max. error vs. Measurement	Max. error vs. Icepak	Runtime	Speedup			
	(sec)	(°C)	(°C)	(sec)	(X)			
C1	41524	1.10	1.65	32.17	1290.89			
C2	40918	0.92	3.50	29.72	1376.97			
P1	34967	1.44	3.90	8.72	4011.36			
P2	37578	1.72	3.65	6.50	5779.45			

Time step in TNS:

C1/C2: 1 sec P1: 1 sec P2: 0.7 sec Speedup > 1290.89 times Maximum error vs. Icepak < 1.72°C Maximum error vs. Measurement < 3.90°C



Transient Results (2/2)



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Transient Results of Phone-nomenon for A Real Case



Conclusion

- This work develops Phone-nomenon, an iterative framework consider heat transfer mechanisms
- The experimental results have verified that Phonenomenon can accurately (less than 3.58% vs. Icepak) and efficiently (1000×) estimate the temperatures of smartphones.
- This work also builds thermal test vehicle and measures the temperatures for validation. And Phone-nomenon can accurately (less than 3.90 °C vs. measurement) estimate those of smartphones.



Thank you for listening Q&A



Reference

[1] D. L. Carroll, H. Y. Lo, and L. I. Stiel. Thermal conductivity of gaseous air at moderate and high pressures. Journal of Chemical and Engineering Data 13.1, pages 53–57, 1968.

[2] F. P. Incropera, D. P. DeWitt, T. L. Bergman, and A. S. Lavine. Principles of heat and mass transfer, seventh edition. John Wiley & Sons, 2013.

